

COLUMBIA RIVER TREATY HYDROELECTRIC OPERATING PLAN

Assured Operating Plan for Operating Year 1984-85

TABLE OF CONTENTS

	Page
INTRODUCTION	1
SYSTEM REGULATION STUDIES	2
DETERMINATION OF OPTIMUM GENERATION IN CANADA AND THE UNITED STATES	3
OPERATING RULE CURVES	6
OPERATING RULES	10
IMPLEMENTATION	13
REFERENCES	15
TABLES	
1. Composite Critical Rule Curve	
2. Composite Assured Refill Curve	
3. Composite Variable Refill Curve	
4. Duncan Flood Control Storage Reservation Curve	
5. Arrow Flood Control Storage Reservation Curve	
6. Mica Flood Control Storage Reservation Curve	
7. Composite Operating Rule Curve	

COLUMBIA RIVER TREATY HYDROELECTRIC OPERATING PLAN

Assured Operating Plan for Operating Year 1984-85

INTRODUCTION

The Treaty between Canada and the United States of America relating to the cooperative development of the water resources of the Columbia River Basin requires that each year an Assured Operating Plan be agreed by the Entities for the operation of the Columbia River Treaty Storage in Canada during the sixth succeeding year. This plan will provide to the Entities information for the sixth succeeding year for planning the power systems in their respective countries which are dependent on or coordinated with the operation of the Canadian storage projects. The data assumed for this Assured Operating Plan will undergo review by the Entities immediately prior to the 1984-85 operating year and such data may be revised to reflect data and criteria current at that time. Should the Entities fail to agree on such revisions, then this Assured Operating Plan will form the basis for the Detailed Operating Plan for 1984-85.

This Assured Operating Plan was prepared in accordance with the Principles and Procedures for the Preparation and Use of Hydroelectric Operating Plans. ¹ It is based on criteria contained in Annex A and Annex B of the Columbia River Treaty, ² Article VII of the Protocol, ³ Terms of Sale, ⁴ and the Columbia River Treaty Flood Control Operating Plan. ⁵

The Assured Operating Plan consists of:

- (a) The Operating Rule Curve for the whole of the Canadian Treaty Storage, including the Critical Rule Curve, Assured Refill Curve, Variable Refill Curves, and the individual project Upper Rule Curves.
- (b) Operating Rules which specifically designate criteria for operation of the Canadian Treaty Projects in accordance with the principles contained in the above references.

A 40-year System Regulation Study⁶ was utilized to develop and test the operating rules and rule curves. It contains the agreed-upon operating constraints such as maximum and minimum project elevations and discharges.

SYSTEM REGULATION STUDIES

In accordance with Annex A, Paragraph 7, of the Treaty, the Columbia River Treaty Operating Committee conducted system regulation studies reflecting Canadian storage operation for optimum generation in both Canada and the United States. Downstream power benefits were computed with the Canadian storage operation based on the operating rules specified herein. There is a reduction of 5.5 average megawatts of average annual usable energy in the Canadian Entitlement of downstream power benefits. This is within the limits specified by the Treaty.

System Regulation Studies for the Assured Operating Plan were based on 1984-85 estimated loads and resources in British Columbia and in the United States Pacific Northwest System. The Entities have agreed that

the 1984-85 Assured Operating Plan would be based on a 40-year streamflow period and an operating year of 1 August to 31 July. Historical flows for the period August 1928 through July 1968, modified to estimated 1984-85 conditions, 7 were used.

The Critical Rule Curve for these studies was determined from

Bonneville Power Administration Study 85-41. The study indicated a 42½
month critical period for the United States system resulting from the

low flows during the period from 16 August 1928 through February 1932.

It was assumed that all reservoirs, both in the United States and Canada,

were full at the beginning of the critical period except where minimum

release requirements made this impossible.

In the studies, individual project flood control criteria were followed. Although only 7.0 million acre-feet of usable storage at Mica is committed for power operation purposes under the Treaty, the studies incorporate Upper Rule Curves designed to evacuate Mica storage up to the full storage of 12 million acre-feet as specified by the Columbia River Treaty Flood Control Operating Plan. Flood Control and Variable Refill Criteria are based on historical inflow volumes.

DETERMINATION OF OPTIMUM GENERATION IN CANADA AND THE UNITED STATES

In order to determine whether optimum generation in both Canada and the United States was achieved in the system regulation studies, the following three quantities were computed for both the Canadian and United States systems:

- (a) firm energy capability
- (b) January peaking capability
- (c) average annual usable secondary energy

In the studies for the 1984-85 Assured Operating Plan the Canadian storage operation was operated to achieve a weighted sum of the three quantities that was greater than the weighted sum achieved under an operation of Canadian storage for optimum generation in the United States alone.

The table on page 5 shows the results from the studies adopted for the 1984-85 Assured Operating Plan and from studies designed to achieve optimum generation in the United States.

The Columbia River Treaty Operating Committee agreed that for the 1984-85 Assured Operating Plan the three quantities would be assigned the following relative values:

Quantity	Relative Value
firm energy capability (Av.MW)	3
January peaking capability (MW)	1
average annual usable secondary	
energy (Av. MW)	2

The three quantities were added after weighting on this basis and there was a net gain to the combined Canadian and United States systems with the study designed for optimum generation in Canada and the United States.

COMPARISON OF ASSURED OPERATING PLAN STUDY RESULTS

		Optimum Generation in Canada and the United States	Optimum Generation in the United States			Net	
		Study No. 85-41	Study No. 85-11	Loss	Gain	Gain	
1.	Firm Energy Capability (Av. MW)						
	U.S. System1/ Canada (Mica + Rev.)2/ 12,410 1,606	12,410 1,589		<u>-</u> <u>17</u>		
	Total (Av. MW)	14,016	13,999	-	17	17	
2.	January Peaking Capacity (MW)						
	U.S. System ³ / Canada (Mica + Rev.	31,488 3,411	31,485 3,419		3 <u>-</u>		
	Total (MW)	34,899	34,904	8	3	(5)	
3.	Average Annual Usable Secondary Energy (Av. MW)						
	U.S. System Canada (Mica + Rev.)	3,404 167	3,386 177	10	18		
	Total (Av. MW)	3,571	3,563	10	18	8	

- U.S. System firm energy capability was determined over the U.S. system critical period beginning 16 August 1928 and ending 29 February 1932.
- 2/ Canadian (Mica + Revelstoke) system firm energy capability was determined over the Canadian system critical period beginning 1 October 1940 and ending 30 April 1946.
- 3/ U.S. system January peaking capability was determined from January 1937.
- Canadian (Mica + Revelstoke) system January peaking capability was determined from second lowest January peak in 40 years of record for the Canadian system.

OPERATING RULE CURVES

The operation of Canadian storage during the 1984-85 Operating Year shall be guided by an Operating Rule Curve for the whole of Canadian storage, Flood Control Storage Reservation Curves for the individual projects, and operating rules for specific projects. The Operating Rule Curve is derived from the various curves described below. These curves are first determined for the individual Canadian projects, which in turn are used to determine Operating Rule Curves for the individual projects which are then summed to yield the Composite Operating Rule Curve for the whole of Canadian storage. This is in accordance with the provision of Article VII(2) of the Protocol.

- (a) <u>Critical Rule Curve</u>. The Critical Rule Curve indicates the end-of-month storage content of Canadian storage during the critical period. It is designed to protect the ability of the United States system to serve firm load with the occurrence of flows no worse than those during the most adverse historical streamflow period. A tabulation of the Composite Critical Rule Curve for the whole of Canadian storage is included in Table 1.
- (b) Refill Curve. The Refill Curve is a guide to operation of Canadian storage which defines the normal limit of storage draft for secondary energy in order to provide a high probability of refilling the storage. In general, the Operating Plan does not permit serving secondary loads at the risk of failing to refill storages and thereby jeopardizing the firm load carrying capability of the system or the Mica generating plant during subsequent years. The end of the refill period is considered to be 31 July.

The Refill Curve is, in turn, defined by two curves as discussed below. In each case, adjustment should be made for water required for refill of upstream reservoirs when applicable.

(1) Assured Refill Curve. The Assured Refill Curve indicates the end-of-month storage content required to assure refill of Canadian storage based on the 1930-31 water year, the system's second lowest historical volume of inflow for the period January through July as measured at The Dalles, Oregon. The tabulation of the composite Assured Refill Curve for the whole of Canadian storage is included as Table 2.

The schedule of outflows is the same as the Power Discharge Requirements used in computing the Variable Refill Curve discussed in (2) below when The Dalles volume runoff is at 80 million acre-feet.

end-of-month storage contents for the period January through July required to refill Canadian storage during the refill period. It was based on historical inflow volume and Power Discharge Requirements determined in accordance with the Principles and Procedures for the Preparation and Use of Hydroelectric Operating Plans. In the system regulation studies the Power Discharge Requirement was made a function of the natural January - July runoff volume at The Dalles, Oregon. In those years when this volume was lower than 80 million acre-feet, the discharge used was that required to meet firm loads while refilling at 80 million acre-feet. In years when the runoff volume at The Dalles exceeded 95 million acre-feet the Power Discharge Requirement was the project minimum outflow. For intermediate volumes the Power Discharge Requirement used in computing the Variable Refill Curves was interpolated linearly between the values shown below:

POWER DISCHARGE REQUIREMENTS IN CFS FOR JANUARY THROUGH JULY VOLUME AT THE DALLES

		80 M	AF			95 MAF			
Project	Jan Feb <u>Mar</u>	Apr	May Jun	<u>Ju1</u>	Jan Feb Mar	Apr	May Jun	Jul	All Periods
Mica	3,000	11,600	11,600	14,600	3,000	3,000	3,000	3,000	3,000
Arrow	5,000	17,500	26,500	43,500	5,000	9,600	9,600	14,000	5,000
Duncan	100	1,700	1,700	1,700	100	900	900	900	100

Composite Variable Refill Curves for the whole of Canadian storage for the 40 years of historical record are recorded in Table 3; the effect of the Limiting Rule Curve, as described below, is included. These illustrate the probable range of these curves based on historical conditions. In the actual operation in 1984-85, the Power Discharge Requirements will be based on the forecast of unregulated runoff at The Dalles.

(c) <u>Limiting Rule Curve</u>. The Limiting Rule Curves indicate monthend storage contents which must be maintained to guarantee the system meeting its firm load during the period January 1 - March 31 in the event that the Variable Refill Curves permit storage to be emptied and sufficient natural flow is not available to carry the load prior to start of the freshet. Such rule curves shall limit the Variable Refill Curve to be no lower than the Limiting Rule Curve. The Limiting Rule Curve shall be developed for 1936-37 water conditions.

- (d) Upper Rule Curve. The Upper Rule Curves indicate end-ofmonth storage content to which each individual Canadian storage project shall be evacuated for flood control and other requirements. The Upper Rule Curves used in the studies were based upon Flood Control Storage Reservation Diagrams contained in the Columbia River Treaty Flood Control Operating Plan and analysis of system flood control simulations. Each Upper Rule Curve is constrained to be not lower than the Variable Refill Curve, except in those years in which the April-August unregulated volume of runoff for the Columbia River at The Dalles exceeds 120 million-acre feet, and Canadian storage is subject to on-call request. Flood control curves for each of the Canadian Treaty projects for the 40-year study period are shown on Tables 4, 5 and 6; however, the tables do not reflect the constraint that the Upper Rule Curve not be lower than the Variable Refill Curve. Tables 5 and 6 reflect an assumed transfer of 2 million acre-feet of flood control storage space from Arrow to Mica. In actual operation, the Flood Control Storage Reservation Curves will be computed as outlined in the Flood Control Operating Plan, using the latest forecast of runoff available at that time.
- (e) <u>Definition of Operating Rule Curve</u>. During the period 1 August through 31 December, the Operating Rule Curve is defined by the Critical Rule Curve or the Assured Refill Curve, whichever is higher. The Critical Rule Curve for the first year of the critical period is used in the foregoing determination. During the period 1 January through 31 July, the Operating Rule Curve is defined by the higher of the Critical Rule Curve and the Assured Refill Curve, unless the Variable Refill Curve is

lower than this value; then it is defined by the Variable Refill Curve. During the period 1 January through 31 March, it will not be lower than the Limiting Rule Curve. The Operating Rule Curve meets all requirements for flood control operation (except as noted in paragraph (d) of the Operating Rules). Composite Operating Rule Curves for the whole of Canadian storage for all 40 years of historical record are included as Table 7 to illustrate the probable future range of these curves based on historical conditions.

OPERATING RULES

The following rules, used in the System Regulation Study, will apply to the operation of Canadian storage in the 1984-85 Operating Year.

- (a) The whole of the Canadian storage may be drafted to its Operating Rule Curve as required to produce optimum generation in Canada and the United States in accordance with Annex A, Paragraph 7, of the Treaty, subject to project physical characteristics, operating constraints, and the criteria for the Mica project listed in (e) below.
- (b) The whole of the Canadian storage will not be drafted below its Operating Rule Curve unless:
- (1) Reservoir storage in the United States system has been drafted to its Energy Content Curve.
- (2) Deliveries of secondary energy in the United States are discontinued.
- (3) Committed firm thermal and miscellaneous resources not displaced by surplus firm hydro resources are in operation or other replacement energy has been secured from sources other than those committed.

- (c) When the conditions of (b) above are met, and it is necessary to draft additional storage to produce optimum generation as determined by the Critical Period System Regulation study, the whole of the Canadian storage and reservoir storage in the United States system will be drafted proportionately between its Operating Rule Curve or Energy Content Curve, respectively, and its Critical Rule Curve. The proportionate draft will be made, if necessary, first to the first year Critical Rule Curve, then between the first and second year Critical Rule Curve, the second and third year Critical Rule Curve, etc. When it is necessary to operate the whole of the Canadian storage and the United States reservoir storage below their lowest Critical Rule Curves, each shall be operated proportionately between its lowest Critical Rule Curve and its normal minimum content, except that Mica Reservoir will continue to be operated in accordance with (e) below, so as to optimize generation at site as well as downstream in the United States. In the event the Mica operation results in less than that project's proportional share of draft from the whole of Canadian storage, compensating drafts will be made from Arrow to the extent possible.
- (d) Mica project will be operated to the target outflow which depends on the end of previous period Arrow storage content shown in the table on page 12 as qualified in (1) to (3) below:
- (1) Mica monthly outflows will be increased in the months from October to June if required to avoid violation of the Upper Rule Curve.
- (2) Mica monthly average outflows will be decreased to minimum if required to avoid withdrawing more than 7 million acre-feet of storage.

MICA PROJECT OPERATING CRITERIA

Month	End of Previous Period Arrow Storage Content (KSFD)	Target Average Outflow (CFS)	Minimum Outflow (CFS)
August 1-15	3,500 - FULL 3,400 - 3,500 0 - 3,400	10,000 15,000 20,000	10,000
August 16-31	3,400 - FULL 3,300 - 3,400 0 - 3,300	10,000 15,000 20,000	10,000
September	3,200 - FULL 3,000 - 3,200 0 - 3,000	10,000 15,000 20,000	10,000
October	3,000 - FULL 2,700 - 3,000 0 - 2,700	10,000 15,000 20,000	10,000
November	3,200 - FULL 2,200 - 3,200 0 - 2,200	15,000 20,000 25,000	10,000
December	2,800 - FULL 2,300 - 2,800 0 - 2,300	25,000 30,000 35,000	15,000
January	2,500 - FULL 100 - 2,500 0 - 100	25,000 30,000 35,000	15,000
February	1,000 - FULL 0 - 1,000	25,000 30,000	15,000
March	200 - FULL 100 - 200 0 - 100	15,000 20,000 25,000	15,000
April 1-15	100 - FULL 0 - 100	15,000 25,000	15,000
April 16-30	300 - FULL 0 - 300	10,000 20,000	10,000
May	200 - FULL 100 - 200 0 - 100	10,000 15,000 20,000	10,000
June	1,400 - FULL 1,100 - 1,400 0 - 1,100	10,000 15,000 20,000	10,000
July	3,000 - FULL 2,700 - 3,000 0 - 2,700	10,000 15,000 20,000	10,000
	1,400 - FULL 1,100 - 1,400 0 - 1,100 3,000 - FULL 2,700 - 3,000	10,000 15,000 20,000	

(3) Under this Assured Operating Plan, Mica storage releases in excess of the 7 million acre-feet that are required to maintain the minimum Mica outflows specified under this plan will be retained in the Arrow reservoir, subject to flood control criteria at Arrow. The total combined storage draft from Mica and Arrow will not exceed 14.1 million acre-feet unless flood control criteria will not permit the additional Mica storage releases for minimum flow purposes to be retained at Arrow. Should storage releases in excess of 14.1 million acre-feet be made, the target Mica outflow will remain as specified in the table on page 12.

Revelstoke has been included in the 1984-85 Assured Operating Plan and has been operated as a run-of-river project.

IMPLEMENTATION

The Entities have agreed that each year a Detailed Operating Plan will be prepared for the immediately succeeding operating year. Such Detailed Operating Plans are made under authority of Article XIV 2.(k) of the Columbia River Treaty which states:

- ". . . the powers and the duties of the entities include:
- (k) preparation and implementation of detailed operating plans that may produce results more advantageous to both countries than those that would arise from operation under the plans referred to in Annexes A and B."

The Detailed Operating Plan for 1984-85 will reflect the latest available load, resource, and other pertinent data to the extent the Entities agreed these data should be included in the plan. Beginning on

I January 1984, the Assured Operating Plan contained herein will be reviewed and the data and criteria updated, as agreed by the Entities, to form the basis for a Detailed Operating Plan for the 1984-85 Operating Year. Failing agreement on updating the Assured Operating Plan, the Detailed Operating Plan will include all data and criteria given in this Assured Operating Plan. Actual operation during the 1984-85 Operating Year shall be guided by the Detailed Operating Plan.

The operating rules to be used in implementation of the Detailed Operating Plan are generally the same as the operating rules described in this document.

The values used in the Assured Operating Plan studies to define the various rule curves were month-end values only. In actual day-to-day operation it is necessary to operate in such a manner during the course of each month that these month-end values can be observed in accordance with the operating rules. Because of the normal variation of power load and streamflow during any month, straight line interpolation between the month-end points should not be assumed.

During the storage drawdown season, Canadian storage should not be drafted below its month-end point at any time during the month unless it can be conservatively demonstrated that sufficient inflow is available, in excess of the minimum outflow required to serve power demand, to refill the reservoir to its end-of-month value as required. During the storage evacuation and refill season, operation will be consistent with the Flood Control Operating Plan. When refill of Canadian storage is being guided by Flood Control Refill Curves, such curves will be computed on a day-by-day basis using the residual volume-of-inflow forecasts depleted by the volume required for minimum outflow from each day through the end of the refill season.

REFERENCES

- Principles and Procedures for the Preparation and Use of Hydroelectric Operating Plans dated 1 May 1979.
- Treaty between Canada and the United States of America relating to Cooperative Development of the Water Resources of the Columbia River Basin dated 17 January 1961.
- ³ Protocol -- Annex to Exchange of Notes dated 22 January 1964.
- 4 Terms of Sale -- Attachment to Exchange of Notes dated 22 January 1964.
- ⁵ Columbia River Treaty Flood Control Operating Plan dated October 1972.
- BPA Hydroelectric Power Planning Program, Assured Operating Plan 40-year System Regulation Study 85-41, dated 14 August 1979.
- Provisional Report on Modified Flows at Selected Sites, 1928 to 1968 for the 1970 and 2020 Level of Development, Columbia River and Coastal Basins, Columbia River Water Management Group, Revision 2, dated April 1974 and May 1974, respectively.
- 8 Summary of End-of-month Reservoir Storage Requirement from Columbia River Flood Regulation Studies dated April 1973 and as updated March 1975.

COLUMBIA RIVER TREATY COMPOSITE CRITICAL RULE CURVES FOR THE WHOLE OF CANADIAN STORAGE FND OF MONTH CONTENTS IN KSFD 1934-85 OPERATING YEAR

	A11G 15	AUG 31	SEP	OCT	NOV	DEC	na L	FEB	MAR	APRIS	APR 30	MAY	JUN	JUL
IST YR	7814.6	7814.6	7806.2	7587.8	7086.1	5817.2	4005.4	2069.3	1812.6	1368.1	1287.9	2739.4	6100.1	7338.6
2ND YR	7691.0	7766.9	7569.4	6985.3	6075.8	4733.4	2450.2	1284.7	1183.5	751.6	884.2	2231.9	4963.9	7071.8
3PD YR	7508.3	7636.9	7560.9	6925.7	6077.1	4499.2	2451.7	1000.7	848.8	373.1	119.9	1559.1	4172.3	5730.7
4TH YR	5842.7	5782.1	5638.3	4892.0	3528.8	1391.4	522.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0

COLUMBIA RIVER TREATY
COMPOSITE ASSURED REFILL CURVE
FOR THE WHOLE OF CAMADIAN STORAGE
END OF MONTH CONTENTS IN KSF0
1984-85 OPERATING YEAR

Table 2

AUG 15	AUG31	SEP	OCT	NOV	DEC	MEL	FEB	MAR	APRIS	APR 30	MAY	JUN	JUL
37.8	330 - 2	1443.8	1779.2	1936.4	2002.7	2060 .4	2092.7	2191.3	2097.1	2107.9	3485.5	6278.5	7814.6

20

15

COLUMBIA RIVER TREATY COMPOSITE VARIABLE REFILL CURVES FOR THE WHOLE OF CAMADIAN STORAGE END OF MONTH CONTENTS IN KSFD 1984-35 OPERATING YEAR

FLOW

	AUG 15	AUG 31	SEP	OCT	NOV	DEC	JAN	FEB	MAR	APRIS	APR 30	MAY	JUN	JUL
1928-29							5376 .4	5328-0	5478.8	5433.6	5388.3	5482.0	6887.8	7814.6
1929-30							3419.0	2993.4	2968.4	3135.1	3301.7	4290.6	6598.6	••
1930-31							3795.0	3549.4	3722.9	3763.0	3803.2	4251.7	6746.2	••
1931-32							1897.4	960.5	221.4	0.0	0.0	612.1	4749.6	••
1932-33							••	••	• •	**	••	597.6	448 9.8	••
1933-34							• •	**	• • •	**	••	930.5	5325.3	••
1934-35							• •	968.2	292.8	193.8	296.1	1739.0	5055.8	• •
1935-36								960.5	247.9	119.3	191.9	1939.7	5793.8	• •
1936-37							5577.3	5523.6	5658.0	5641.1	5624.2	5663.4	6906.2	• • •
1937-38							1897 -4	960.5	221.4	14.8	29.7	1612.4	5138.5	**
1938-39							3443.9	3017-1	3108.5	3205.2	3301.8	4129.8	6891.9	••
1939-40							2944.9	2530.5	2583.5	2778.8	2974.0	3806.3	6714.5	• •
1940-41							4408.5	4323.2	4544.8	4790.7	5036.6	5628.1	6962.6	• •
1941-42							2106.5	1656.2	1612.6	1704.2	1795.8	3033.4	5865.8	••
1942-43							1897.4	1277.8	1202.1	1424.5	1646.9	3122.0	5635.7	• •
1943-44							6367.7	6135.6	6052.5	5972.9	5893.2	6062.3	7121.9	• • •
1944-45							5423-2	5365.1	5575.0	5561.2	5547.5	5619.8	6931.0	,,
1945-46							1897.4	960.5	221.4	0.6	0.0	613.7	4967.0	••
1946-47							••	**	• •	**	• •	1338.3	5144.4	• • •
1947-48							••	••	• •	•••	•••	795.7	4950.5	• • •
1948-49							1991.8	1432.3	1077.0	1418.0	1793.9	3149.9	6381.6	••
1949-50							1897.4	960.5	221.4	9.0	0.0	970 . 1	4378.0	• • •
1950-51							••	••	* *	••	• •	1355.3	5240.1	••
1951-52							•••	**		28.7	57.4	1786.8	5379.3	• • •
1952-53							• •	**	333.6	485.2	657.3	2047.0	5302.0	• • •
1953-54							**	**	221.4	0.0	8.0	286.4	4327.7	• • •
1954-55							••		••	23.4	46.8	1367.3	4508.8	••
1955-56							••	**	• •	0.0	0.0	1050.5	5043.4	. ,,
1956-57							• •	**	• •	• • •	• •	911.9	5514.6	• • •
1957-58							••	••	••	•••	•••	723.6	5106.6	• •
1958-59							•••	•••	• •	**	**	473.8	4429.6	• • •
1959-60							**	• • •	• •	107.0	213.8	1638.6	4840.8	• •
1960-61							• • •	•••	,,	0.0	0.0	527 . 6	4738.5	• •
1961-62							• •	•••	• • • • • • • • • • • • • • • • • • • •	262.2	307.5	1742.2	5079.2	• • •
1962-63							••	•••	• •	110.8	220.9	1857.9	5169.4	• •
1963-64							•••	•••	• • •	0.0	0.0	576.3	4155.6	• • •
1964-65							• • • • • • • • • • • • • • • • • • • •	•••	• • •	56.9	113.7	1675.1	5053.4	• • •
1965-66							• • • • • • • • • • • • • • • • • • • •	**	229.9	44.9	61.0	1154.1	5002.8	
1966-67							• • •		221.4	C. 0	0.0	37.0	3694.6	
1967-68							• •	• • •	• • •	•••	•••	383.3	4278.8	
									..	• •				• •

FLOOD CONTROL STORAGE RESERVATION CURVES DUNCAN

KSFD 1984-85 OPERATING YEAR

	AUG 15	AUG 31	SEP	OCT	VON	DEC	JEN	FEB	MAR	APELS	APR30	MAY	JUN	JUL
1928-29	705.8	705.8	705.8	705.8	735.8	504.1	397-2	303.0	303.0	311.0	324.6	415.4	560.6	705.8
1929-30	**	• •	• • •		• • •	,,	385.7	281.3	281.3	289.9	304.6	400 . 8	553.0	••
1930-31	**	• •	• • •	* * *		• •	368.5	248.0	248.0	257.1	272.7	377.1	540.9	
1931-32	••	• •	* *		• •	• • •	272.2	65.5	65.5	80.6	108.9	281.3	609.5	• • •
1932-33	• •	• • •	• • •	• •		• • •	**	•••	,,	75.1	94.2	191.5	573.2	• •
1933-34	••	• •	,,	• •	,,	• •	• •	••	• •	65.5	127.0	339.8	605.5	• •
1934-35	• • •	• • •	••	• • •	•••	•••	• •	•••	• • •	•••	83.7	187.0	488.0	
1935-36	•••	• • •	**		• • •	• •	**	**	• • •	71.1	119.5	351.9	705.8	••
1936-37	••	• • •	• • •	• •	• • •	• • •	353.9	219.8	219.8	229.4	246.0	356.9	530.9	•••
1937-38	• •	• • •	,,	,,	•••	,,	272.2	65.5	65.5	77.1	83.7	217.3	542.4	•••
1938-39	**	• • •	•••	• • •	• • •	**		**	•••	82.6	107.4	385.7	705.8	••
1939-40	••	• •	• •	• •	• • •	,,		•••	11	78.1	103.8	••	••	••
1948-41	•••	• • •	• • •	;;	• • •	,,	321.1	156.3	156.3	167.3	186.0	311.0	508.2	•••
1941-42	**		7.7		• • •	• • •	302.0	121.0	121.0	131.0	155.2	291.9	483.0	• • •
1942-43	**	• • •	• • •	• •	• • •	•••	305.0	126.0	126.0	141-1	172.9	248.0	647.8	• •
1943-44	,,		• • • • • • • • • • • • • • • • • • • •	;;			392.7	294.4	294.4	302.5	316.6	410.4	557.6	
1944-45	• •	• •	• • •		••	,,	361.5	234.4	234.4	235.9	236.9	349.9	567.7	•••
1945-46	.,,	• • •	• • •	• •	• • •		272.2	65.5	65.5	75.6	95 . 8	322.1	647.3	• • •
1946-47	• • •		**	;;			•••	**	,,	77.1	101.8	314.1	629.7	
1947-48	• • •			**			;;			65.5	65.5	300.4	705.8	
1948-49	•••		• • •	• • •	,,	• • • • • • • • • • • • • • • • • • • •	348.3	208.7	208.7	215.2	236.9	408.8	**	• • •
1949-50	;;		• • •		• • • • • • • • • • • • • • • • • • • •		272.2	65.5	65.5	72.1	84.7	184.0	525.3	• • •
1950-51	• • •	• •		,,	• • •	,,	**	•••	•••	79.6	103.3	285.3	534.4	••
1951-52	,,	• • •	**		• • •	**	• • •	**	,,	65.5	67.5	92.2	255.1	• • •
1952-53	;;	• • • • • • • • • • • • • • • • • • • •	• • • • • • • • • • • • • • • • • • • •		;;	;;		;;	;;	72.1	84.7	234.4	522.8	;;
1953-54	• • •	.,	• • •		,,	,,			,,	73.1	84.2	236.9	547.5	•••
1954-55	**	**	**	,,	**	,,	**	• • •	,,	72.1	80.6	154.7	488.5	• • •
1955-56	;;		• • •	;;	;;		;;	26.7	26.7	26.7	26.7	239.9	578.2	;;
1956-57	;;			;;	• • •			65.5	65.5	74.6	89.7	376.1	655.9	
1957-58	**	**			•	**		11		77.1	96.3	359.4	705.8	• • • • • • • • • • • • • • • • • • • •
1958-59	;;	::	::				::		::	65.5	65.5	129.5	513.7	;;
1959-60	::		**	• •	::	••	•••	••	•••	"	•••	161.3	545.5	;;
1960-51	**	•••	• •	• •	••	**	••	•••	••			193.6	705.8	
1961-62		"	• • •	• • •	**	**	• • •	• • • • • • • • • • • • • • • • • • • •	::	**	78.1	1,3500	545.5	**
1962-63	•••	••	• • •	• •	• • • • • • • • • • • • • • • • • • • •	• • •	• • •	• • •	••			;;	,,,,,	
1963-64	••	**	• •	• •	• • •	• •	••	•••	••	••	65.5	161.3	513.7	**
1964-65	•••	• • •	• •	• • •	• • •	• • •	••	• •	• •	••	129.5	225.3	545.5	• • •
1965-66	••	• • •	• • •	• •	• • •	••	••	• • •	••	•••	97.3			• • •
1966-67	••	• •	• •	••	• •	••	• •	••	• •	• •	65.5	193.6	577.7	• • •
1967-68	••	••	• •	•••	• • •	•••	,,	• •	••	••			513.7	**
1401-00	* *	• •	• •	• •	• • •	• •	• •	**	* *	* *	• • •	• •	213.7	• •

Table 4

FLOOD CONTROL STORAGE RESERVATION CURVES

KSFD 1964-85 OPERATING YEAR

	AUG 15	AUG 3 I	SEP	OCT	NOV	DEC	JAN	FER	MAR	APE15	APR 30	HAY	JUN	JUL
1928-29	3579.6	3574.6	3579.6	3453.5	3453.6	3075.4	3875 -4	3075.4	3075.4	3088.5	3111.2	3235.8	3579.6	3579.6
1929-30	* *	• •			• •	**	3060.8	3347.7	3033.1	3047.2	3071.9	3207.0	**	* *
1930-31	••	,,	• •	• •	• •	••	3075.4	3375.4	₹075.4	3068.5	3111.2	3235.8	**	
1931-32		• •	1:1		11	• •	2364 .6	1719.2	1008.3	1015.9	1126.8	2224.4	• • •	
1932-33	* *	• • •	* * *			**	***	**	,,	1008.3	1036.6	1761.6	3034.6	
1933-34	••		• •		• •	• •	••		••	• • •	1784.8	2327.2	3579.6	• • •
1934-75					• •	• • •		• • •	**	• •	1008.3	1725.8	3034.6	
1935-36	, ,	• •	,,		* *	**		• • •	,,	1069.9	1373.4	2134.7	3579.6	• •
1936-37	• •		• •				2998.3	2927.7	2850.6	2869.7	2902.5	3082.5	••	
1937-38	••	,,	• •	• •		• • •	2364.6	1719.2	1008.3	1283.0	1278.1	1831.1	3147.5	• •
1938-39		* *	• •	,,	9 9	• •	2637.8	2243.6	1805.9	1869.5	1983.4	2735.1	3579.6	. ,,
1939-40	,,		,,		,,	,,	2849.6	2645.4	2420.0	2454.8	2536.0	2999.8	••	* *
1940-41		,,		,,	• •	,,	3075.4	3275.4	3075.4	3088.5	3111.2	3235.8	• •	••
1941-42	• •		* * *	• •	• •	• •	2364.6	1719.2	1008.3	1064.8	1149.5	1934.0	**	
1942-43	• •	• •		,,	• •	• •		• •	• • •	1111.2	1321.9	1440 -4	2389.3	• •
1943-44	**		* *		• •	•••	3075.4	3075.4	3075.4	3088.5	3111.2	3235.8	3579.6	• •
1944-45		**	• •	,,	• •	,,	2641.8	2251.6	1818.0	1842.7	1908.3	2477.0	3368.4	**
1945-46	• • •	• •	,,		,,	• • •	2364.6	1719.2	1008.3	1072.4	1242.3	2201.2	3579.6	• • •
1946-47	,,	••		• • •	.,	• • •			•••	1075.4	1360.8	2147.3	•••	• • •
1947-48	**			• • •		• •	,,	**	• • •	1036.6	1183.3	2216.8	**	• • •
1948-49	• •	• •	•••		• •	• • •	• •	• •	• •	1144.5	1375.9	2494.6	•••	,,
1949-50	••	••	,,	• •	• •	• • •	• •	• •	,,	1103.6	1113.7	1113.7	2232.5	• •
1950-51	• • •	**		• • •	• •	• • •	**	• • •	,,	1052.2	1101.1	1355.2	3338.1	• • •
1951-52	• •	• • •	• •		• •	• • •	**	••	• •	1069.9	1345.1	1792.3	3013.9	• •
1952-53	••	••	,,	,,		• • •		••	•••	1057.3	1172.7	1476.2	••	,,
1953-54	• • •	• • •	• • •	• • •	* *	**	1.7	**	• • • • • • • • • • • • • • • • • • • •		1134.4	1628.0	1898.2	• • •
1954-55	••	• •	• • •	• •	• •	• • •	• •	• • •	• •	1075.4	1090.5	1653.7	3224.7	• •
1955-56	,,	• •	• •	• •	,,	,,	.,	857.1	0.0	0.0	289.9	1367.3	2763.4	••
1956-57	• •		•••	• • •		• • •	,,	1719.2	1008.3	1077.9	1224.1	2651.4	3579.6	• • •
1957-59	**	•••	• •	• •	• •	• • •	••	••	••	164E.7	1190.9	2242.5	"	**
1958-59	,,	• • •		,,	.,	• •	,,	• • •	• •	1008.3	1008.3	1394.0	3322.5	••
1959-60			• • •	,,	• •	• • •	• •	,,	• • •	• •	• • •	1779.7	3579.6	
1960-61	• •		• • •	• • •	,,	• • •	**	• • •	• • •	••	• • • • • • • • • • • • • • • • • • • •	1651.2	"1	**
1961-62		.,	• • • • • • • • • • • • • • • • • • • •	• • •	,,	• • •	• •	.,		• •	::	2036.8	3322.5	;;
1962-63	••	.,	,,	• • •	• • •	,,	2484.5	1950.1	1359.2	1359.2	1359.2	1914.3	3579.6	• • •
1963-64	**	(9))	• • •	**	• •	**	2364.6	1719-2	1006.3	1008.3	1008.3	1265.5	3322.5	
1964-65	• • • • • • • • • • • • • • • • • • • •					,,	,,	**	,,,	**	•••	1651.2	3579.6	
1965-66	;;	;;	;;	;;	;;	::	2528.4	2034.8	1487.8	1487.8	1487.8	2324.7	997 988	::
1966-67	**	• • •	• • •		• • • • • • • • • • • • • • • • • • • •	• • • • • • • • • • • • • • • • • • • •	2364.6	1719.2	1008.3	1008.3	1008.3	1394.0	3322.5	
1967-68		;;	";	;;	;;	;;	2367.1	1723.1	1015.4	1015.4	1015.4	1528.6	3579.6	
		* *	* *		7.7	7.7	C 001			141204		1 250 0	331 300	* *

Table 5

FLOOD CONTROL STORAGE RESERVATION CURVES

KSFD

1984-85 OPERATING YEAR

AUG 15 AUG31 SEP OCT NOV DEC FEB MAR APRIS APR30 MAY JUN JUL JAN 1928-29 3529.2 3428.4 3406.7 3387.0 3365.3 3369.9 3380.5 3412.2 3469.7 3529.2 3529.2 3529.2 3428.4 3428.4 1929-30 3378.5 3332.6 3282.7 3290.2 3305.9 3353.2 3440.0 1930-31 3428.4 3428.4 3428.4 3431.4 3437.9 3457.1 3492.9 1931-32 3149.6 3100.7 2808.2 2480.5 2511.8 2577.8 2781.5 •• . . ., •• .. 1932-33 1933-34 ., •• 1934-35 1935-36, .. , , 3353.2 3208.5 3218.1 3238.3 3300.8 3413.2 1936-37 3233.7 1937-38 3100.7 2808.2 2480.5 2511.8 2577.8 2781.5 3149.6 1938-39 3213.1 3018.5 2836.7 2828.4 2873.8 3013.9 3267.5 • • 3353.2 3057.3 3182.3 1939-40 3296.8 3174.3 3042.7 3088.1 1940-41 3428.4 3428.4 3428.4 3431.4 3437.9 3457.1 3492.9 2577.8 3149.6 1941-42 3100.7 2808.2 2480.5 2511.8 2781.5 ,, . . ,, 1942-43 ** 3431.4 3437.9 3457.1 3492.9 1943-44 3428 .4 3428.4 3428.4 3021.5 2878.3 3017.5 32€9.6 1944-45 3214.6 2811.3 2832.9 1945-46 3100.7 2808.2 2480.5 2511.8 2577.8 2781.5 3149.6 1946-47 99 1947-48 ,, .. ,, ,, 1948-49, .. 1949-50, 1950-51 1951-52 ,, 1952-53, .. ., 1953-54 .. • • ** ., ,, * * ,, 1954-55 100.9 803.7 2363.6 1955-56 3025.0 2067 .1 1258.8 100.9 100.9 2577.8 2781.5 3149.6 1956-57 3428.4 3100.7 2808.2 2480.5 2511.8 ,, ,, 1957-58 1958-59 .,, 1959-60 . . ** .. • • ,, ., ,, ., •• ,, ., .. 1960-61 • • 1961-62 2654.0 2710.4 2885.9 3202.5 1962-63 3150.6 2902.1 2626.7 ., 2781.5 3149.6 1963-64 3100.7 2838.2 2480.5 2511.8 2577.8 .. ,, 1964-65 3221.7 2936.3 2680.2 2705.9 2759.3 2923.7 1965-66 3168.7 . . ,, ,, 1966-67 3100.7 2808.2 2480.5 2511.8 2577.8 2781.5 3149.6 2783.5 3131.7 2810.3 2483.6 2514.8 2580.9 3150.6 1967-68

Table 6

COLUMBIA RIVER TREATY COMPOSITE OPERATING RULE CURVES FOR THE WHOLE OF CAMADIAN STORAGE END OF NONTH CONTENTS IN KSFD 1984-85 OPERATING YEAR

FLOW

	AUG 15	AUG 31	SEP	OCT	NOV	DEC	JAN	FEB	MAR	APRIS	APR 30	HAY	JUN	JUL
1928-29	7814.6	7814.6	7806.2	7587.8	7086.1	5817.2	4137.3	2443-1	2191.3	2097.1	2107.9	3485.5	6526.5	7814.6
1929-30	* *	••	••	* *	**	**	3209.9	2164.9	2173.6	**	• •	• •	6505.2	• •
1939-31		• •	• •	• •	• •	• • •	3641.3	2443.1	2191.3	,,	,,	,,	6526.5	• •
1931-32	**	• •	••	• •	••	• •	1897.4	960.5	221.4	0.0	0.0	612.1	4749.6	• •
1932-33	• •		• •	••	• •	••	••	**	• •	••	••	597.6	4409.0	• • •
1933-34	*10	* *	* *	41	* *	,,		**	• •	**	• • •	930.5	5325.3	* *
1934-35	• •	• •	• •		••	•••	• •	968.2	292.8	193.8	296.1	1739.0	50 55.8	••
1935-36	••	• •	• •			* *	• • •	960.5	247.9	119.3	191.9	1939.7	5793.8	
1936 - 37	• •	• •	* *	• •	• •	* *	4137.3	2443.1	2191.3	2097.1	2107.9	3485.5	6526.5	• •
1937-38	• •		••	• •	• •	••	1897-4	960.5	221.4	14.8	29.7	1612.4	5138.5	• •
1938-39	* *		• •	• •	• •	**	3435.7	2322.4	2158.1	207€.2	2093.7	3447.5	6526.5	• •
1939-40	• •	• •		• •	• •	**	2944-9	2185.0	2154.2	2078.3	2101.9	3449.7	••	• •
1940-41	• •	* *			**	**	4076.4	2443.1	2191.3	2097.1	2107.9	3485.5	••	• •
1941-42	* *	• •	• •	,,	• •	**	2106.5	1656.2	1448.6	1561.1	1740 - 4	3033.4	5865.4	
1045-47	• •		• •			**	1897.4	1277.8	1202.1	1424.5	1646.9	3152.7	5635.7	
1943-44	• •	• •	• •			• •	4137.3	2443.1	2191.3	2097.1	2107.9	3485.5	6526.5	* *
1944-45	• •		••	••	• •	**	**	••	• •	**	••		••	• •
1945-46	• •		**	* *	• •	• •	1897.4	960.5	221.4	0.0	0.0	613.7	4967.0	***
1946-47	• •		••	• •	• •	••	**	••	* *	••	••	1338.3	5144.4	**
1947-49	• •	• •	• •	* *	••	* *	**	••	• •	**	• •	795.7	4950.5	••
1948-49	• • •		••	• •	• •	• •	1991.8	1432.3	1977.0	1263.0	1487.9	2897.9	6188.1	• •
1949-50	• •	• •	••	• •	••	••	1897.4	960.5	221.4	9.6	0.0	970.1	4378.0	• •
1950-51	• •	• •	• •	,,	• •	**	• • •	**	• •	**	• • •	1355.3	5240.1	• •
1951-52	• •	• •	• •			• •		• •	,,	28.7	57.4	1785 . 8	5379.3	**
1952-53	• •	* *	***		• • •	• •	• •	• •	333.6	485.2	657.3	2047.0	5302.0	• •
1953-54	• •	• •	• •	* *	• •	**	**	••	221.4	0.0	0.0	286.4	4327.7	••
1954-55	• •	••	• •		**	• •	**	••	••	23.4	46.8	1367.3	4508.8	• •
1955-56	• •		• •	* *	• •	**	**	• •	••	0.0	0.0	1050.5	5043.4	• • •
1956-57	• •	• •	••	• •	••	• •	**	••	• •	**	••	911.9	5514.6	••
1957-5A	,,		,,	* *	• •	• • •	• •	• •	• • •	**	• • •	728.6	5106.6	* *
1958-59	• •	• •	••	• •	• • •	• •	• •	••	••	••	• •	473.8	4429.6	• •
1959-60	• •	• •	• •	• •	* *	• •	••	••	• •	107.0	213.8	1638.6	4840.8	• •
1960-61	• •	* *	• • •	• •	••	• •	• •	••	• •	0 • C	0.0	527.6	4738.5	• • •
1061-65	••	• •		••	• •	• • •	••	••	• •	205.5	307.5	1742.2	5079.2	• •
1962-63	***	• •		• •	• •	• •	• •		**	110.8	220.9	1857.9	5169.4	• •
1963-64	**	• •	• • •	• •	• •	••	• •	••	• •	0.0	0.0	576.3	4155.6	• •
1964-65	**	• •	••	• •	• •	• •		••	••	56.9	113.7	1675 . 1	5053.4	• •
1965-66	• •	• •	• • •	• •	• •	• •	**	• • •	229.9	44.9	61.0	1154.1	5002.8	
1966-67	••	• •	• •		• •	• •	• •	••	221.4	C • 0	0.0	37.0	3694.6	• •
1967-68	••	• •	• •	• •	••	• •	••	• •	• •	• •	• •	383.3	4278.8	* *

DETERMINATION OF DOWNSTREAM POWER BENEFITS RESULTING FROM CANADIAN STORAGE FOR OPERATING YEAR 1984-85 September 1979

Introduction.

The Treaty between Canada and the United States of America and related documents relating to the cooperative development of the water resources of the Columbia River Basin require that downstream power benefits from Canadian storage be determined in advance by the two Entities. The purpose of this report is to set out the results of downstream power benefit computations for the sixth succeeding year, 1984-85, and for the storage for which the Assured Operating Plan was developed.

The procedures followed in the benefit studies are those provided in Annex A, Paragraph 7; in Annex B of the Treaty; in Articles VIII, IX, and X of the Protocol; and in the document, "Columbia River Treaty Principles and Procedures for Preparation and Use of Hydroelectric Operating Plans," dated May 1979 (POP).

The Canadian Entitlement Benefits were computed as follows:

- Step I based on the total U.S. planned hydro and thermal system with 15½ maf of Canadian storage operated for optimum generation in both countries (85-41 study).
- Step II based on the U.S. base hydro and thermal system with 15½ maf of Canadian storage operated for optimum generation in both countries (85-42 study).
- Step III- based on the U.S. base hydro and thermal system operated for optimum generation in the U.S. (84-13 study).

As part of the determination of downstream power benefits for the operating year 1984-85, separate determinations were carried out relating to the limit of year-to-year change in benefits attributable to the operation of Canadian storage in operating plans designed to achieve optimum generation at-site in Canada and downstream in Canada and the United States of America.

II. Results of Study.

(a) The Canadian Entitlement, which is one-half the total computed downstream power benefits, was computed to be:

> Dependable Capacity = 1,438.5 MW Average Annual Energy = 544.5 MW

(b) One-half of the downstream power benefits determined for 15 maf of Canadian storage operated for optimum generation in the United States was computed to be:

> Dependable Capacity = 1,413.0 MW Average Annual Energy = 545.0 MW

In accordance with Part III, Paragraph 15c(2) of POP, the minimum permitted downstream power benefits for the 1984-85 operating year are as follows:

Dependable Capacity = 1,446.5 - (1,446.5 - 1,413.0) = 1,413.0 MWAverage Annual Energy = 536.0 - (541.0 - 545.0) = 540.0 MW

The above computations are based on the formula X - (Y - Z), where the quantities X, Y, and Z are defined in POP. The quantities X and Y are derived from the downstream power benefit computations set out in the 1983-84 agreement. The computed downstream power benefits exceed these amounts.

III. Effect on Canadian Entitlement.

The Canadian Entitlement to downstream power benefits was sold to the United States of America under the Canadian Entitlement Purchase Agreement dated 13 August 1964. By definition, the Canadian Entitlement for 1984-85 Assured Operating Plan had been designed to achieve optimum generation downstream in the United States alone. The Canadian Entitlement determined for the conditions above would have been:

Dependable Capacity = $\frac{1}{2}$ of 2,877 MW or 1,438.5 MW Average Annual Energy = $\frac{1}{2}$ of 1,100 MW or 550.0 MW

Since the 1984-85 Assured Operating Plan was in fact designed to achieve optimum generation at-site in Canada and downstream in the United States of America, Section 7 of the Agreement requires that "any reduction in the Canadian Entitlement resulting from action taken pursuant to Paragraph 7 of Annex A of the Treaty shall be determined in accordance with Subsection (3) of Section 6 of this Agreement." The Canadian Entitlement of downstream power benefits under the 1984-85 Assured Operating Plan was determined as:

Dependable Capacity = $\frac{1}{2}$ of 2,877 MW or 1,438.5 MW Average Annual Energy = $\frac{1}{2}$ of 1,089 MW or 544.5 MW

The comparison indicates a reduction in Canadian Entitlement of 5.5 average megawatts of average annual usable energy, but no reduction in dependable capacity. This reduction would be in respect of the period 1 April 1984 through 31 March 1985 in accordance with POP.

The Entities are agreed that the United States Entity is entitled to receive during the period 1 April 1984 through 31 March 1985, from B.C. Hydro & Power Authority, 5.5 average megawatts of energy in accordance with Sections 7 and 10 of the Canadian Entitlement Purchase Agreement dated 13 August 1964.

IV. Computation of Entitlement.

The following Tables and Charts are attached and summarize the study:

Table 1. Computation of Canadian Entitlement

The essential elements used in the computation of the Canadian Entitlement as provided in Paragraphs 2 and 3 of Annex B are shown in this table.

Table 2. Summary of Power Regulations for the Computation of Canadian Entitlement to Downstream Benefits.

This table summarizes the Step I, II, and III regulations by projects.

Table 3. Determination of Load Shape for Steps II and III,
Canadian Entitlement Computation

The load shape for Steps II and III carry the same ratio between each month and the annual average as does the Pacific Northwest area load. The Northwest area firm loads on this table were based on the current forecast data. The Grand Coulee pumping load is also included in this estimate.

The firm load for Steps II and III is computed as follows:

- Estimate the hydro nominal prime power for the critical period;
- (2) Add the thermal from Step I less reserve;
- (3) Multiply (2) by the ratio of the area annual average firm load to the area critical period firm load to obtain the annual average firm load for Steps II and III (the ratios used in this study were 0.98654 and 0.95366, respectively);
- (4) Pro rate the average annual Step II and III load determined in (3) by months in the ratio that each monthly area load bears to the annual average area load; and

(5) Subtract the thermal in each month to obtain the monthly firm hydro load. The average annual hydro loads for Steps II and III also become the firm energy considered usable according to Annex B, Paragraph 3(a).

Charts 1 & 2. Secondary Energy Duration Curve, Steps II and III

These charts are duration curves of the secondary energy for Steps II and III. The secondary energy is the capability each month which exceeds the firm hydro loads shown in Table 3. The usable secondary energy shown in average megawatts for each step is computed in accordance with Annex B, paragraphs 3(b) and 3(c). The "other usable secondary" was computed on the basis of 40 percent of the remainder after thermal replacement. The thermal replacement was limited to the existing and scheduled thermal energy capability after allowance for reserve and minimum thermal generation, except when an energy surplus condition occurs; then the thermal replacement must not exceed the total of the thermal energy required to supply firm plus the estimated secondary load.

Thermal Energy Capability - MW	8,324	1/
Less Minimum Thermal Generation	1,619	
Thermal Replacement - MW	6,705	

The following tabulation shows the ordinate values for usable secondary energy:

	Step II	Step III
Thermal Replacement	6,705	6,705
Other	1,630	2,388
Total - MW	8,335	9,093

Thermal energy capabilities are based on an annual plant factor of 60 percent the first full year of operation and 75 percent thereafter. These annual plant factors include deductions for energy reserves and scheduled maintenance.

COMPUTATION OF CANADIAN ENTITLEMENT 1984-1985

Generation Figures are in Average Megawatts; Load Factors, in Percent

Determination of Dependable Capacity Credited to Canadian Storage	
Critical Period Average Rate of Generation with Canadian Storage, Step II Critical Period Average Rate of Generation without Canadian Storage, Step III Gain Due to Canadian Storage	9,075 7,054 2,021
Estimated Average Critical Period Load Factor Percent	70.253
Dependable Capacity Gain 1/	2,877
Canadian Share of Dependable Capacity	1,438.
Determination of Increase in Average Annual Usable Energy Step II (with Canadian Storage)	
Annual Firm Hydro Energy	2,275
Step III (without Canadian Storage)	
Annual Firm Hydro Energy	3,330 565
Average Annual Usable Energy Gain	,089
Canadian Share of Average Annual Energy Gain	544.5

Dependable capacity gain credited to Canadian storage equals gain in critical period average rate of generation divided by the estimated average critical period load factor.

	BASIC DATA STEP I						Step II				STEP III			
		Nominal			Critical -	Critical			Critical					
PROJECTS	Number of Units	Installed Peaking Capacity MM	Usable Storage 1000 AF	January Peaking Capability MW	Period Average Generation MW	Unable Storage 1000 AF	January Peaking Capability MW	Period Average Generation HW	Average Annual Generation	Usable Storage 1000 AF	January Peaking Capability MW	Period Average Generation MW	Average Annual Generation MW	
CANADIAN														
Mica Arrow Duncan Subtotal			7,000 7,100 1,400 15,500			7,000 7,100 1,400 15,500								
BASE FEDERAL SYSTEM		Y	-											
Hungry Horse Albent Falls Grand Coules Chief Joseph Les Harbor McNary John Day The Dalles Bonneville Subtotal	4 3 24 + 2 27 6 14 16 22 18	328 49 6,415 2,412 693 1,127 2,484 2,018 1,114 16,640	3,161 1,155 5,185 535	235 24 6,389 2,412 693 1,127 2,484 2,018 1,114 16,496	96 2,001 1,086 215 638 921 816 608 6,406	3,008 1,155 5,072 9,235	241 23 6,380 2,412 693 1,124 2,484 2,018 1,114 16,489	115 22 1,770 1,000 222 590 922 794 590 6,025	102 22 2,372 1,323 302 755 1,258 1,035 734 7,903	3,008 1,155 5,072 9,235	280 24 5,951 2,412 693 1,124 2,484 2,018 1,114 16,100	212 25 1,227 712 170 430 684 633 466 4,359	101 25 2.278 1.250 302 711 1.225 1.015 704 7.611	
BASE SYSTEM NON-FEDERAL		5			9									
Kootenay Lake (Canadian) Kerr Thompson Falls Noxon Rapids Cabinet Gorge Box Canyon Coeur d'Alene & Long Lake Wells Chelan Rocky Reach Rock Island Manapan Priest Rapids Brownlee Ozhow Subtotal	3 6 5 4 4 10 2 11 18 10 10 4 4	160 40 554 230 74 820 54 1,267 544 986 912 675 220 6,536	649 1,219 231 327 677 980 4,083	151 40 546 230 71 820 51 1,267 544 986 912 675 220 6,513	112 36 148 106 46 436 38 589 278 356 529 205 87 3,166	427 1,219 223 676 974 3,519	151 40 554 230 71 820 51 1,267 544 986 912 675 220 6,521	101 38 138 93 45 408 38 552 261 523 497 246 108 3,050	114 32 211 123 48 510 46 711 329 657 617 269 115 3,780	427 1,219 223 676 974 3,519	150 40 554 230 71 820 51 1,267 544 986 912 675 220 6,520	139 37 158 106 51 289 49 394 183 367 358 250 114 2,495	116 32 211 124 48 471 44 668 303 599 566 260 116 3,558	
TOTAL BASE SYSTEM HYDRO		23,176	29,619	23,009	9,572	28,254	23,010	9.075	11,683	12,754	22,620	7,054	11,169	
ADDITIONAL STEP 1 PROJECTS					-57									
Libby Rereg. Boundary Spokame River Plants Hells Canyon Dworshak Lower Granite Little Goose Lover Monumental Pelcon and Round Butte Subtotal	8 3 3 6 6	966 88 655 153 450 460 930 930 930 454 6,016	2,015 2,015 274 7,223	666 88 655 151 438 429 930 930 930 930 437 5,654	187 35 360 89 170 163 215 215 214 124 1,772									
Independent Resources		4,857	8,352	4,107	1,754									
TOTAL HYDRO RESOURCES		34,049	45,194	32,770	13,098									
MISCELLANEOUS CONTRACTS		-	-	23	9									
THERMAL RESOURCES 1/ Small Existing Thermal Pl Centralia #1 & #2 Jim Bridger #1, #2, #3, 4 Colstrip #1 & #2 Trojan Boardman MSP #2 Colstrip #3 & #4 MSP #1 WSP #3 WSP #3 Added Thermal Requirement				1,444 1,313 2,000 330 1,130 530 1,130 840 1,220 0 2,773	176 962 1,431 255 824 405 796 591 821 286 113 1,664									
TOTAL THERMAL RESOURCES				12,680	8,324									
TOTAL IMPORTS				100	464									
ESTIMATED HYDRO MAINTENANCE TOTAL RESOURCES (HYDRO AND				-678 44,895	-30 21,865									
RESERVES 2/	.HERVAL)			-2,806	0									
RESOURCES AVAILABLE FOR LOA	D			42,089	21,865									
ESTIMATED LOAD				and the same of	X2247.60									
Pacific Northwest Area				35,077	21,865					24				
SURPLUS OR (DEFICIT)				7,012	0									
CRITICAL PERIOD Starts: Ends: Length (Months): Study Identification				August 16, February 1: 42% Months 85-41	932		0	September 1943 April 1945 20 Montha 85-42		Apr	otember 16, 1936 :11 15, 1937 Sonths 85-13		.1	

Thermal energy capabilities are based on an annual plant factor of 60 percent the first full year of operation and 75 percent thereafter. These annual plant factors include deductions for energy reserves and scheduled maintenance.

^{2/} Peak reserves are 8 percent of peak load; energy reserve deductions have been included in thermal plant energy capability.

DETERMINATION OF LOAD SHAPE FOR STEPS II AND III 1984-85 CANADIAN ENTITLEMENT COMPUTATIONS

	Pacific Nort		Step II		Step III				
	Peak	Avg.	Load Factor %	Total Firm Load 1/	Thermal Firm Load	Hydro Firm Load	Total Firm Load 1/	Thermal Firm Load	Hydro Firm Load
		11/81		<u> 2000</u> 1/	Load	Dodd	Hoad I/	Load	Load
Aug. 1-15	28,142*	19,759	70.21	15,584	8,324	7,260	13,315	8,324	4,991
Aug. 16-31	28,064*	19,579	69.77	15,442	8,324	7,118	13,193	8,324	4,869
Sept. 1-15	28,390*	19,135	67.40	15,092	8,324	6,768	12,894	8,324	4,570
Sept. 16-30	28,345*	19,097	67.37	15,062	8,324	6,738	12,868	8,324	4,544
October	30,049*	20,251	67.39	15,972	8,324	7,648	13,646	8,324	5,322
November	32,067*	22,722	70.86	17,921	8,324	9,597	15,311	8,324	6,987
December	34,587*	24,628	71.21	19,424	8,324	11,100	16,595	8,324	8,271
January	35,077*	25,339	72.24	19,985	8,324	11,661	17,075	8,324	8,751
February	33,201*	23,984	72.24	18,916	8,324	10,592	16,162	8,324	7,838
March	31,494*	22,691	72.05	17,896	8,324	9,572	15,290	8,324	6,966
Apr. 1-15	29,694*	21,216	71.45	16,733	8,324	8,409	14,296	8,324	5,972
Apr. 16-30	30,036*	21,336	71.03	16,828	8,324	8,504	14,377	8,324	6,053
May	29,868*	20,383	68.24	16,076	8,324	7,752	13,735	8,324	5,411
June	29,628*	20,681	69.80	16,311	8,324	7,987	13,936	8,324	5,612
July	29,050*	20,537	70.70	16,197	8,324	7,873	13,839	8,324	5,515
Critical Period Avg.		21,865	70.253	17,399	8,324	9,075	15,378	8,324	7,054
Annual Average		21,764		17,165	8,324	8,841	14,665	8,324	6,341
January Peak	35,077*								
Step I Critical Period Aug. 16, 1928 -			Critical	Period Se	ept 1943-	Critical	Period Se	pt. 16,	
3.79	Feb. 29, 1932					or. 1945			r. 15, 193
42½ Months					20	Months		7 Mo	nths

Total firm load of Step II and Step III systems, computed for each system to have an average energy load equivalent to the average energy capability within the critical period and to bear a constant ratio, month by month, to the Pacific Northwest Area Load.

^{*} Figures so marked are peak megawatts. All other figures are monthly or semi-monthly energy in average megawatts.



